

MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A BASED ON THE EXACT AND NORMAL APPROXIMATIONS TO THE BINOMIAL DISTPIBUTION

Research Report No. 82-6

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Carlos Amado Richard S. Leavenworth Richard L. Scheaffer

RESEARCH REPORT



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Industrial & Systems
Engineering Department
University of Florida
Gainesville, FL. 32611

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ACCEPTANCE CONTROL CHARTS BASED ON THE EXACT AND NORMAL APPROXIMATIONS TO THE BINOMIAL DISTRIBUTION

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by

Carlos Amado Richard S. Leavenworth Richard L. Scheaffer

December 1982

Department of Industrial and Systems Engineering University of Florida Gainesville, Florida 32611

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ABSTRACT

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TABLE OF CONTENTS

	PAGE
ABSTRACT	. i
INTRODUCTION	. 1
PROBLEM FORMULATION: EXACT BINOMIAL	. 2
PROBLEM FORMULATION: NORMAL APPROXIMATIONS	. 5
PROBLEM SOLUTION: NORMAL APPROXIMATIONS	. 9
ANALYSIS	. 12
SIMULATION STUDY	. 21
CONCLUSIONS	. 27
REFERENCES	. 30
APPENDIX	. a1

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Procedures are developed for finding the sample size and control limit for Acceptance Control Charts for proportion of nonconforming units using the exact binomial distribution, the standard normal approximation to the binomial, and a normalized arcsin transformation of the data. The user must select an Acceptable Process Level and a Rejectable Process Level and the associated risks for each. The approximation methods are compared to the exact method over a wide range of design specifications. It was found that the arcsin transformation is considerably more accurate than the standard normal approximation and, although more complex to figure, is preferable if the user is familiar with small scientific pocket calculators. If a microprocessor or minicomputer is available, the exact binomial may be used with ease to achieve at least the stipulated risk protection desired. FORTRAN programs for the three formulations are included.

ACCEPTANCE CONTROL CHARTS BASED ON THE EXACT AND NORMAL APPROXIMATIONS TO THE BINOMIAL DISTRIBUTION

INTRODUCTION

The control chart for fraction rejected, or p-chart, probably is the most widely used of all control chart procedures. It may be applied to one or more than one quality characteristic whether measured on a go, not-go, basis or as variables measurements. So long as the result of an inspection is to classify an item as meeting specifications (acceptable) or not meeting specifications (unacceptable), a single p-chart may be used.

When the sample subgroup size is constant, the chart for \underline{np} may be used conveniently since it records the actual count of rejected units in a subgroup of size \underline{n} rather than the proportion rejected. In either case, the binomial probability density function may be used to model the process.

The standard Shewhart control chart for <u>np</u> places the upper and lower control limits at:

$$n\overline{p} + 3\sqrt{n\overline{p}(1-\overline{p})}$$

where:

 \overline{np} is the average count of rejected units for a series of subgroups of constant size, n.

$$\sqrt{n\overline{p}(1-\overline{p})}$$
 is the standard deviation of the binomial count (σ_{np}) .

Thus these limits are standard 3-sigma limits of the Shewhart control chart. While variation beyond these limits at random should occur very rarely indeed, the same probabilities often associated with random variation beyond 3 sigma limits on an \overline{X} chart should not be applied. Nevertheless, exact probabilities

calculated from the binomial distribution may be found for $\frac{np}{np}$ control charts with 3-sigma limits or any other set of limits which are a multiple of σ_{np} .

In the case of the Acceptance Control Chart, at each point a sample is selected a decision is to be made either to accept the hypothesis that the process is operating as specified, at the acceptable quality level or better, or that the actual quality level is beyond an acceptable level (a higher value of \underline{p}). The decision criterion is the upper control limit on np, $\underline{np} + \underline{Z}\gamma \ \underline{q_{np}}, \text{ where } \gamma \text{ is the probability of acceptance of the hypothesis}$ with respect to \underline{p} using a normal approximation to the binomial distribution. (\underline{Z} equals 3 for the standard Shewhart control chart.)

This paper explores the development of Acceptance Control Charts for binomial counts of the number of units rejected. Two parameters are to be found, one the value of the control limit, and the second, the appropriate (constant) sample size, \underline{n} .

The problem is formulated in three ways, using the exact binomial distribution, using a standard normal approximation to the binomial, and using a normalized arcsin transformation. Analytical results of application of the three methods are compared and the results of a simulation study using computer-generated synthetic data are presented.

PROBLEM FORMULATION: EXACT BINOMIAL

If samples are being drawn from a continuous process generating nonconforming items at a constant rate, \underline{p} , the binomial distribution describes this process accurately. The probability density function is

$$f(r|n,p) = {n \choose r} p^r (1-p)^{n-r}$$
 (1)

where r = no. of units rejected

n = sample (or subgroup) size.

The probability that the number of units rejected is less than or equal to some fixed value, \underline{c} , is:

$$P[r < c|n,p] = \sum_{r=0}^{c} {n \choose r} p^{r} (1-p)^{n-r} = \gamma$$
 (2)

Limits for acceptance control charts, like acceptance numbers for sampling plans, usually are designed by selecting two points on an Operating Characteristic (OC) curve, as illustrated in Figure 1. One point assures that an Acceptable Process Level (APL), p_1 , has a high probability of being accepted of at least 1- α ; the other assures that a Rejectable Process Level (RPL), p_2 , will have a suitable low probability of acceptance of at most β . α and β are the design risk levels associated with the process quality levels p_1 and p_2 , respectively, where p_2 is greater than p_1 .

The two equations needed should express the fact that it is desired that the OC curve pass through, or pass as close as possible to, the two points specified as the design criteria, namely, $(\underline{p_1},1-\alpha)$ and $(\underline{p_2},\beta)$. These equations are:

$$P[r < c | n, p_1] = \sum_{r=0}^{c} {n \choose r} p_1^r (1-p_1)^{n-r} > 1-\alpha$$
 (3)

$$P[r < c|n,p_2] = \sum_{r=0}^{c} {n \choose r} p_2^r (1-p_2)^{n-r} < \beta$$
 (4)

They are expressed in inequality form because, for any integer values of \underline{n} and \underline{c} , it is unlikely that the cumulative probability can exactly satisfy $1-\alpha$ and β . As the result there are an infinite number of $(\underline{n},\underline{c})$ pairs satisfying (3) and (4) above some minimum combination. The complete formulation thus requires the further stipulations:

where:
$$p_2 > p_1$$
 and $1-\alpha > \beta$ (5)

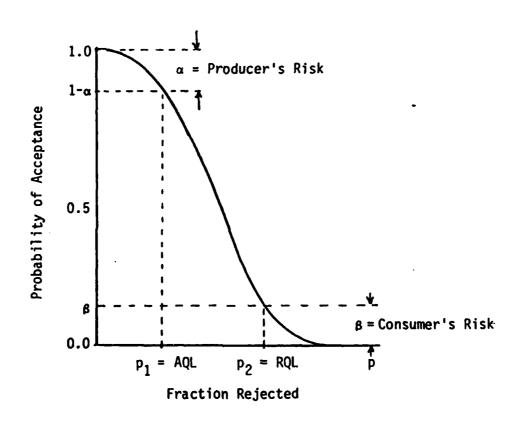


Figure 1. Design Operating Characteristic (OC) Curve for np Chart.

Referring to Fig. 1, equation (3) assures that the resulting OC curve will pass above and to the right of the design curve at the point $(\underline{p}_1, 1-\alpha)$. Equation (4) assures that the resulting OC curve will pass below and to the left of the point (\underline{p}_2,β) . Stipulating the choice of the minimum $(\underline{n},\underline{c})$ pair assures that the resulting OC curve passes as closely as possible to the design curve.

The value of \underline{n} , of course, yields the constant subgroup size to be used in sampling. Thus the \underline{np} chart becomes a reasonable and easily understandable alternative to the \underline{p} chart. The value of \underline{c} is the maximum count of rejected units that should lead to \underline{no} corrective action on the process. Only if $(\underline{c}+1)$ or more units are rejected should action be taken. However, if the Acceptance Control Limit (ACL) is plotted exactly at the value of \underline{c} , the user may become confused as to whether or not to take action. In accordance with the rules of control chart interpretation, this is not a coin-flip situation. A reasonable procedure is to plot the Acceptance Control Limit at:

$$ACL = c + 0.5 \tag{6}$$

thus avoiding any confusion in chart interpretation.

PROBLEM FORMULATION: NORMAL APPROXIMATIONS

Working with the binomial formula presents a number of mechanical problems some of which are discussed subsequently. Suffice it to say at this point in the discussion that no closed form solution for the values of <u>n</u> and <u>c</u> exists. Its application involves repetitive use of some form of search algorithm. Therefore no one should be surprised that considerable attention and ingenuity have been applied in the development of useful approximations to the cumulative binomial.

Johnson and Kotz (1969) provide a rather extensive survey of binomial approximation techniques and Raff (1956) has compared the accuracy of several of them. The two presented and compared in this study are the standard normal approximation and a normalized arcsin transformation. The standard normal approximation is the most familiar and used as alluded to in the Introduction. It is easy to apply since \underline{n} and \underline{c} may be obtained directly with the use of a slide rule or pocket calculator and a table of the standard normal curve. The arcsin transformation is somewhat more complicated but easily adaptable for use on a programmable pocket calculator.

Standard Normal Approximation

The mean and standard deviation of the binomial distribution are:

$$E(r) = np$$

$$\sigma_r = \sqrt{np(1-p)}.$$

The distribution of the standardized binomial variable

$$Z = (r-np)/\sqrt{np(1-p)}$$

tends to the standard normal distribution as \underline{n} becomes large. (See Johnson and Kotz, 1969.) That is, for any real number, X:

$$\lim_{N\to\infty} P[Z < X] = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{X} exp(-u^2/2) du$$

which values may be found in a table of the normal curve or solved for on many programmable pocket calculators. Thus, if given the value of an ACL (say, derived from the exact binomial, non-integer, and equal to $\underline{c} + 0.5$), the probability of \underline{c} or less occurrences with \underline{n} and \underline{p} known, $\underline{\phi}(\underline{Z})$, requires only the calculation of:

$$Z_{\gamma} = (ACL-np)/\sqrt{np(1-p)}$$
 (7)

and $\Phi(Z_{\gamma}) = \gamma$ from a cumulative (left-hand) normal curve table.

Arcsin Transformation

The arcsin transformation

$$y = \sin^{-1} \sqrt{(r + 3/8)/(n + 3/4)}$$

produces a random variable, \underline{y} , which is approximately normally distributed. (See Johnson and Kotz, 1969.) Thus a normalized random variable, Z, produces a statistic, the asymptotic distribution of which is normal, where:

$$Z_{\gamma} = 2\sqrt{n} \left[\sin^{-1} \sqrt{\frac{c + 3/8}{n + 3/4}} - \sin^{-1} \sqrt{p} \right]$$
 (8)

and $\Phi(Z_{\gamma}) = \gamma$ is then found on a cumulative normal curve table.

PROBLEM SOLUTION - EXACT BINOMIAL

Restating the problem, the objective is to find an $(\underline{n},\underline{c})$ pair such that:

minimize: n,c

subject to:

$$P[r < c|n,p_1] > 1-\alpha$$
 (3)

$$P[r < c|n,p_2] < \beta$$
 (4)

where:

$$p_1 < p_2 \text{ and } \beta < 1-\alpha.$$
 (5)

Guenther (1969) develops a search procedure for finding $(\underline{n},\underline{c})$ pairs that satisfy equations 3, 4, and 5*. While Guenther's algorithm is aimed at

^{*}Actually Guenther's paper is devoted to finding sample sizes (n) and acceptance numbers (c) for single sampling acceptance plans. The procedure, however, is the same. In his paper, the hypergeometric, binomial, and Poisson distributions are used.

deriving plans by hand calculation and the use of tables, it is an iterative, brute-force technique more amenable to computerization than to hand calculation.

Hailey (1980) programmed Guenther's algorithm to find the minimum single sampling acceptance plan satisfying equations (3) and (4). His paper contains the FORTRAN IV computer code for deriving plans using either the binomial distribution or the Poisson.

The algorithm operates basically as follows. For any stipulated value of \underline{c} , there is a minimal sample size, \underline{n} , satisfying equation (4). That value is designated $\underline{n}_{\underline{s}}$, a minimal value of \underline{n} . For the same value of \underline{c} , there also exists a maximum value of \underline{n} satisfying equation (3). That value is designated $\underline{n}_{\underline{s}}$, a maximum value for \underline{n} . If the solved value of $\underline{n}_{\underline{s}}$ is less than the solved value of $\underline{n}_{\underline{s}}$ for fixed \underline{c} , no feasible solution exists for that value of \underline{c} or any lesser value. If $\underline{n}_{\underline{s}}$ is greater than (or equal to) $\underline{n}_{\underline{s}}$, then any value of $\underline{n}_{\underline{s}}$ (a unique solution) is the range $\underline{n}_{\underline{s}} < \underline{n} < \underline{n}_{\underline{s}}$ is feasible for that value of \underline{c} . In fact, feasible solutions exist for any value of \underline{c} greater than the designated value, as well. That is, an infinite number of plans exist satisfying equations (3) and (4).

The search procedure begins by setting \underline{c} equal to zero and solving for $\underline{n}_{\underline{s}}$ and $\underline{n}_{\underline{\ell}}$. The value of \underline{c} is increased by one and the process repeated until a feasible range of \underline{n} is found. Hailey's program immediately selects the minimum \underline{n} , $\underline{n}_{\underline{s}}$, and terminates with a series of output options. A variation of this program was used to derive sample sizes and ACL's based on the binomial distribution. The sample size, \underline{n} , was set equal to $\underline{n}_{\underline{s}}$ and the Acceptance Control Limit

ACL = c + 0.5

in order to avoid any confusion in the interretation of points falling on the control limit.

PROBLEM SOLUTION: NORMAL APPROXIMATIONS

Hand calculation using the algorithm stated in the previous section would become most tedious and time-consuming. Available tables of the binomial may not cover the ranges of \underline{n} or \underline{p} required. To evaluate the binomial where \underline{c} equal 50 requires the calculation and summing of 51 terms, which is a large task even with the aid of a sophisticated pocket calculator or small computer. This procedure would have to be repeated many times before the minimum $(\underline{n},\underline{c})$ pair are found. However, approximations usually require the evaluation of only two equations one for \underline{n} and one for \underline{c} .

Standard Normal Approximation

If Z_{α} denotes the value that cuts off an upper tail area of α under the standard normal curve, as illustrated in Figure 2, then the acceptance plan $(\underline{n},\underline{c})$ pair can be found from the following equations:

$$Z_{1-\alpha} = \frac{c - n p_1}{\sqrt{n p_1 (1-p_1)}}$$

$$-Z_{1-\beta} = \frac{c - n p_2}{\sqrt{n p_2 (1-p_2)}}$$

Solving these equations simultaneously yields:

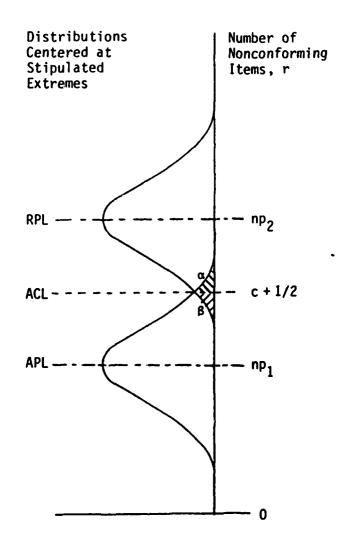


Figure 2. Acceptance Control Charting Scheme for Binomial Counts.

$$n = [(Z_{1-\alpha} \sqrt{p_1(1-p_1)} + Z_{1-\beta} \sqrt{p_2(1-p_2)})/(p_2-p_1)]^2$$
 (9)

$$c = Z_{1-\alpha} \sqrt{n p_1(1-p_1)} + n p_1$$
 (10)

$$= -Z_{1-\beta} \sqrt{n p_2(1-p_2)} + n p_2$$

The values of \underline{n} and \underline{c} may be calculated rather quickly by hand or by the use of a programmable pocket calculator. This is the simplest formulation of the problem. The value of \underline{n} , of course, is rounded to the nearest integer.

Arcsin Transformation

The acceptance control chart plan $(\underline{n},\underline{c})$ pair can be found by solving the following equations:

$$Z_{1-\alpha} = 2 \sqrt{n} \left[\sin^{-1} \sqrt{\frac{c + 3/8}{n + 3/4}} - \sin^{-1} \sqrt{p_1} \right]$$

$$-Z_{1-\beta} = 2\sqrt{n} \left[\sin^{-1} \sqrt{\frac{c + 3/8}{n + 3/4}} - \sin^{-1} \sqrt{p_2} \right]$$

Solving these two equations simultaneously yields:

$$n = \{ (Z_{1-\alpha} + Z_{1-\beta}) / [2 (\sin^{-1}\sqrt{p_2} - \sin^{-1}\sqrt{p_1})] \}^2$$
 (11)

$$c = (n + 3/4) \left\{ \sin \left[Z_{1-\alpha}/(2\sqrt{n}) + \sin^{-1}\sqrt{p_1} \right] \right\}^2 - 3/8$$
 (12)

Again, the value of <u>n</u> is rounded to the nearest integer. The derived function $\sin^{-1}(x) = \tan^{-1}(x/\sqrt{1-x^2})$ may be used to obtain the inverse sin of x, where -1 < x < 1, in computers which do not have an inverse sin function, (Standard Mathematical Tables, 1973).

ANALYSIS

The three methods of calculating $(\underline{n},\underline{c})$ pairs for Acceptance Control Charts were investigated using the popular risk levels of α equals 0.05 and β equals 0.10. The value of \underline{p}_1 ranges from 0.005 to 0.06 in increments of 0.005. The value of \underline{p}_2 changes iteratively in order to maintain specified levels of the discrimination ratio, $\underline{D} = \underline{p}_2/\underline{p}_1$. The value of \underline{D} ranges from 1.5 to 5.0 in increments of 0.5.

Acceptance Control Chart plans in terms of $(\underline{n}, \underline{c})$ pairs are presented in Table 1. The three methods are labeled BINOMIAL, NORMAL, and ARCSIN to identify, respectively the cumulative binomial distribution, standard normal approximation, and normalized arcsin transformation.

Subgroup sizes, the \underline{n} 's, obtained from the two approximations, ARCSIN and NORMAL, have been rounded to the nearest integer. The acceptance control limits, the \underline{c} 's, where not converted to integers because values from these approximations yield different risk protections depending on whether a continuity correction is added or subtracted from \underline{c} before it is converted. For example:

Acceptance Control Limit (Integerized)		Truncate Value of	Risk Protection Favored
c'	=	c + 0.5	Type I error
С	=	С	Inconsistent
C*	=	c - 0.5	Type II error

where 0.5 is a continuity correction implicit in Laplace's Theorem. (See Johnson and Kotz, 1969, p.53.) Thus, the conversion of \underline{c} to integer is performed after determining the continuity correction which will yield the type of risk protection most favorable to the quality control program.

	P.1.4	0.0050			0.0100			0.0150		
METHOD	Ω	Ç	c	ť	ř	c	ť	6	c	ť
Bikomial Arcsine Kormal	r. s	0.0075	8474.0 8428.0 8218.0	53.00 53.09 51.61	0.0150	4163.0 4188.0 4083.0	52.00 52.77 51.29	0.0225	2774.0 2774.0 2705.0	52.00 52.44 50.98
Bindhial Arcsine Normal	5.0	0.0100	2473.0 2478.0 2373.0	18.00 18.47 17.52	0.0200	1235.0 1230.0 1178.0	18.00	0.0300	822.0 814.0 779.0	18.00 18.21 17.26
Bindhial. Arcsine Kormal	٠. ب	0.0125	1230.0 1258.0 1188.0	10.00	0.0250	614.0 623.0 588.0	10.00 10.62 9.85	0.0375	409.0 412.0 389.0	10.00
Birohial Arcsine Kormal	3.0	0.0150	783.0 792.0 739.0	7.00	0.0300	390.0 392.0 366.0	7.00 7.46 6.78	0.0450	260.0 259.0 241.0	7.00
Binomial Arcsine Normal	ب د	0.0175	600.0 559.0 517.0	3.3.0	0.0350	299.0 276.0 255.0	5.74	0.0525	175.0 182.0 168.0	3.00 3.73
Bindhial Arcsine Normal	o.	0.0200	462.0 423.0 388.0	844 084 044	0.0400	198.0 209.0 191.0	4.76 4.78	0.0400	132.0 138.0 126.0	4.00 4.71 4.13
Bindhial Arcsine Normal	r: *	0.0225	354.0 336.0	4.00 3.11 3.56	0.0450	176.0 166.0 151.0	4.00 4.07 3.51	0.0675	117.0 109.0	4.00 4.00 4.00 4.00
Bindhial. Arcsinf Korhal	c is	0.0250	266.0 277.0 250.0	3.61 3.61 80.8	. 0500	132.0 136.0 123.0	3.00 3.03 5.03	0.0750	86.0 80.0	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8

Table 1 (a). Acceptance Control Chart Parameters Obtained by Three Methods.

	ë e	0.0200	•	•	0.0250		,	0.0300		,
METHOD	R	2	c	U	2	c	U	2	c	
Binohial. Arcsine Wormal.	r:	0.0300	2043.0 2068.0 2016.0	51.00 52.11 50.66	0.0375	1633.0 1643.0 1662.0	51.00	0.0450	1360.0 1361.0 1327.0	51.00 51.46
Birchial. Arcsine Mormal.	5.0	0.0400	616.0 606.0 580.0	18.00 18.08 17.14	0.0300	492.0 481.0 460.0	18.00 17.95 17.01	0.0600	410.0 398.0 380.0	
Binohiai. Arcsine Kormal	, ic	0.0500	306.0	10.00	0.0625	244.0 243.0 229.0	10.00 10.37 9.60	0.0750	203.0	
Bindhial Arcsine Mormal	3.0	0.0400	192.0	7.33	0.0750	152.0	7.27	0.0900	129.0 126.0 116.0	
Bindhial Arcsine Norhal	80 10	0.0700	131.0 135.0 124.0	5.00 5.63 5.03	0.0875	104.0	8.64.0 64.0	0.1050	87.0 88.0	
bindrial Arcsine Normal	¢.	0.0800	98.0 102.0 93.0	1.00	0.1000	78.0 81.0 73.0	7.00 7.00 7.00 7.00	0.1200	66.0 60.0	
Bindhiol Arcsine Normal	<u>د</u> د	0.0900	87.0 81.0 73.0	00.4 7.00 7.00 7.00 7.00 7.00 7.00 7.00	0.1125	70.0 64.0 57.0	3.95	0.1350	58.0 52.0 47.0	
Bindrial Arcsine Normal	e.	0.1000	65.0 56.0 59.0	3.30	0.1250	52.0 44.0	3.00	0.1500	33.0	

Table 1 (b)

	Pla	0.0350			0.0400			0.0450		
METHOD	Q	~	c	ť	5	c	ť	~	c	ť
Bindhial Arcsine Mormal	٠.	0.0525	1155.0	51.00 51.14 49.71	0.000	1001.0 1007.0 982.0	50.00 50.81 49.39	0.0675	889.0 890.0 867.0	50.00 50.48
Bindhial Arcsine Norhal	0.0	0.0700	334.0 338.0 323.0	17.00 12.69 16.76	0.0800	292.0 294.0 281.0	17.00 17.56 16.63	0.0900	259.0 259.0 247.0	17.00 17.43 16.50
Bindhial Arcsine Kormal	ю 6	0.0875	174.0 170.0 160.0	10.20	0.1000	152.0 148.0 139.0	10.00	0.1125	135.0 130.0 122.0	10.00
Bindhial Arcsine Mormal	e n	0.1050	110.0	7.00 7.14 6.46	0.1200	96.0 92.0 85.0	7.00 7.08 6.39	0.1350	85.0 75.0	7.00
Bindhial Arcsine Normal	10 10	0.1225	74.0 75.0	t: t: 4 € t: 0 € t: 0	0.1400	65 55 59 50 50 50 50 50 50 50 50 50 50 50 50 50	5.00	0.1575	57.0 57.0 52.0	5.00
Bindhial Arcsine Morkal	0.	0.1400	38.00	44 k 900 900 900 900 900 900 900 900 900 90	0.1600	444 00.4	4.00	0.1800	44k 600	44.E
Bindhial Arcsine Kormal	4 IC	0.1575	000 000 000	3.28 3.28	0.1800	33.0 34.0 0.0	3.82	0.2025	333.0	4.00 3.78 3.19
Bindhial Arcsine Horhal	80 O	0.1750	37.0 36.0	24.0	0.2000	32.0 31.0 27.0	3.33 2.73	0.2250	23.0	3.33

Table 1 (c

	P. 1.	0.0500			0.0550			0.040.0		
METHOD	e	۴	c	U	۲۵	c	ť	2	c	Ŀ
Bindhial. Arcsine Normal	t.	0.0750	795.0 775.0	50.00 50.16 48.76	0.0825	713.0 718.0 700.0	49.83 49.83	0.0900	654.0 654.0 638.0	49.50 49.50
Birchial. Arcsine Kurmal	2.0	0.1000	253.0 231.0 221.0	17.00 17.29 16.37	0.1100	212.0 209.0 199.0	17.00 17.16 16.25	0.1200	194.0	17.00 17.03 16.12
binomial arcsine Kormai.		0.1250	121.0	10.00 9.95 9.18	0.1375	110.0 105.0 98.0	10.00 9.86 9.10	0.1500	100.0 95.0 89.0	10.00 9.78 9.01
Birchial Arcsine Normal	c m	0.1500	77.0 72.0 67.0	7.00 6.95 6.26	0.1650	65.0 65.0	7.00 6.88 6.19	0.1800	53.0	7.00 6.82 6.13
Bindhial. Arcsine Normal	in m	0.1750	50.0 50.0 46.0	5.00 5.36 4.71	0.1925	444	88.4 6.40 6.40 6.40 6.40	0.2100	42.0	6.0.4 6.0.6 6.0.6
Bindhial Arcsine Normal	0.	0.2000	33.0 34.0	4.00	0.2200	660 660	3.72 3.72 3.72	0.2400	32.0 31.0 27.0	4.30 3.67
Bindhial Arcsine Normal	٠. د:	0.2250	28.0 30.0 26.0	3.00 3.74 3.14	0.2475	27.0	3.69 3.69 3.09	0.2700	23.0	2.63 8.64
Bindhial Arcsine Korhal	c in	0.2500	22.0 24.0	3.00 3.27 2.68	0.2750	23.0	3.00	0.3000	21.0 19.0 17.0	3.19

Table 1 (d).

For all three methods, \underline{n} and \underline{c} decrease as the difference between the AQL $(\underline{p_1})$ and RQL $(\underline{p_2})$ increases. This can be observed by either maintaining a constant discrimination ratio $(\underline{D} = \underline{p_2}/\underline{p_1})$ and increasing $\underline{p_1}$, or by maintaining a constant $\underline{p_1}$ and increasing \underline{D} .

Tables 2, 3, and 4 indicate the risk over-protection, or under-protection (negative values), which each plan provides. The table values are the differences between actual (P[k < c|p]) values and stipulated ($1-\alpha$ or β) risk protection probabilities. The actual probabilities were obtained using a FORTRAN program, in single precision mode, on a PDP 11/34 computer. The probabilities obtained from this program compared with published binomial probability tables [N.B.S. (1950), Romig (1953), and Harvard (1955)] with an 0.00001 accuracy.

Binomial Distribution

As evidenced in Table 2, ACC plans obtained from the binomial distribution over-protect both the producer and consumer by having low probabilities of committing Type I or Type II errors; i.e., rejecting good quality products or accepting bad quality products. The largest difference between actual and stipulated probabilities is 2.21%. The over-protection is due to the fact that since \underline{n} and \underline{c} are both integers, an OC curve usually cannot pass exactly through points $(\underline{p_1}, 1-\alpha)$ and $(\underline{p_2}, \beta)$, thus the search procedure finds the minimum \underline{n} and \underline{c} which satisfy inequalities (3) and (4).

Standard Normal Approximation

The acceptance control plans obtained from the standard normal approximation generally have smaller subgroup sizes, \underline{n} , than the plans obtained from the other two models. As evidenced in Table 4, this method consistantly protects against Type II error when $\underline{c*}$ is used, but the underprotection

8		ŀ	3 1	22	2	æ		C	9	-		>			٥	9	;	c	ď	9		æ	2		ţ
0.0600			2000	0000	0.01;	0.019		70.0	č o	00.0					0.00	0			0.00	C		0.01	0.0030		
0.0550		1000		1400.0	0.0100	0.0147	1000	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	0.0087	0.0242		2012			0000.	0.00.4	2000	C	0.0011	A 000		0.0103	0.0124		ニメイン・ン
0.0500		8100.0		A500.0	0.0093	0.0115	0000	2000	0.0103	0.000	0.010	6.17			0.0012	0.0011	000	440044	0.0073	0.000		\$100.0	0.0037	0100	212777
0.0450		2.000.0	2000		0.00H1	0.0123	0.0075		0.00.0	0.0231	0.0144				\$000°C	0.0002	0.0041	4 P 3 A 3	0.0018	0.0020		\$100.0	0.0074	7100.0	
0.0400		900000		21000	C/37.3	0.0112	0.0044		E/33.3	0.0221	0.0123				B00000	00000	0.0031		0.0022	0.0074	474	21000	0.0072	0.00.0	
0.0350		0.0029	A 100.0		CC.	0.010%	0.0048	0 0	25000	0.0220	0.0104			0000	70000	5000°0	0.0026		0.0018	0.0033	0000	2022	0.00.0	.0.00BA	
0.0300		0.0022	9400.0	200	****	0.0088	0.0029	4400		0.0201	0.0105	: :		.000	*****	0.0017	0.0011	8000	A 200 C	0.0020	0.0071	V (**/)	0.0068	0.0038	
0.0250		0.0001	0.0047	2.00		0.0083	0.0032	0.0040		2410.0	0.0091			0000	¥ 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0000	900000	9,00	E 700 0	0.0000	A000.0		9900.0	0.0037	
0.0200		0.0004	0.0053	0.00.0		*/00.0	0.0013	0.0027	10.0	94749	9800.0			1,000.0		10000	0.0013	6000		0.00.0	50000		0.0012	0000.0	
0.0150	-ري	0.0013	0.0048	0.0029	0700	20000	00000	C.000.5	0.0170		0.0062			0.0004		7000	0.0014	0.00.0		67666	0.0028		4700.0	0.0038	
0.0100	R= PEKCA P.1.1 - (1-0)	0.0008	0.0035	0.0023	A 200		0.0178	0000.0	0.0172		0.0058	•	TK40 P21	0.000	4000 C		00000	0.000	7000	9000	40000	0,00	00000	9.00B	
0.0050	R. PEKC	0.0004	0.0029	0.0011	5700°0		1/10·0	0.0199	0.0142		0.0042	•	R: 15 - 15	0.0001	0.000		70000	0000.0	A000.0		4000.0	0000		0.00.0	
٦/	, i	r:1	٠. د.	2.5	3.0			c •	4.55		0.0			1.5	2.0		3	c m	V.		0.4			٠ د	

BINOMIAL distribution risk protection difference (R) between actual (P[k<c|p]) and stipulated (1-a or B) probabilities of acceptance plans in Table 1. Table 2.

			•									
_ pl	0.0030	0.0100	0.0150	P.0700	0.0250	0.0300	0.0350	0.0400	0.0450	0.0500	0.0550	0.0400
6												
1.5		<c' +13 -<br="">-0.0017</c' +13>		e'= (c	+0.5) tr		0.0077	-0.0025	0.0032	0.0081	-0.0022	6.0020
7.0				0.0030	EA00.0	0.0033	0.0127	0.0147	0.0164	-0.0031	0.0011	0.0045
2.5	0.0073	0.0131		0.0173	0.0175	0.0217	~0.0058	-0.0032	0.0007	0.0033	0.0044	0.0073
3.0		0.0174		0.0215	0.0240	0.0240	-0.0072	-0.0041	-0.0017	0.0003	0.0040	0.0082
3.5	0.0025	0.0055		0.0110	0.0133	0.0147	0.0162	0.0178	0.0212	0.0237	0.0263	0.02A2
4.0	0.0030	0.0040		0.0106	0.0138	0.0140	0.0175	0.0175	0.0231	0.0241	0.0273 0.0150	0.0273
4.5 5.0	0.0303 0.0122	0.031& 0.0144		-0.00 08	-0.0043 0.0273	-0.0021 0.0234	0.0033 0.0253	0.0043 0.0285	0.005R	0.0113	0.0730	0.015 7 0.0334
	•			4.4173	0.027.	V102.17	4.44.00	010200	0.0200	414411	710010	•.•
	R-B -	PERCE" P										
1.5	-0.0182	-0.0021	-0.0075	-0.0188	-0.0014	-0.0071	-0.0178	-0.0003	-0.0087	-0.0141	0.0004	-0.0044
2.0 2.5	-0.0384 -0.0243	0.0007	-0.0047	-0.0100	-0.0144	-0.0235	-0.0304	-0.0347	-0.0453	-0.000R	-0.0077	-0.0133
3.0	-0.0259	-0.0204	-0.0351	-0.0417	-0.0175	-0.0542	0.0017	-0.0017	-0.00ER	-0.0122	-0.01R4	-0.0234
3.5	-0.0337	-0.0404 -0.0140	-0.0475 -0.0204	-0.0527 -0.0274	-0.0425 -0.0323	-0.0704 -0.034 7	0.0055 -0.0457	-0.0027 -0.0484	-0.0051 -0.0317	-0.0074 -0.0407	-0.0144 -0.0724	-0.0238 -0.0813
4.0	-0.0116	-0.0172	-0.0201	-0.0259	-0.0337	-0.0388	-0.0408	-0.0463	-0.0413	-0.0417	-0.0788	-0.0883
4.5	-0.0804	-0.0842	0.0077	0.0037	-0.0036	-0.0055	-0.0175	-0.0141	-0.0145	-0.0318	-0.0427	-0.0413
5.0	-0.0270	-0.0317	-0.0407	-0.0463	-0.0544	-0.0574	-0.0443	-0.0623	-0.0780	-0.0717	-0.0703	-0.1017
		-1										
1.5	-0.0104	(c p1) - (-0.0017	-0.0174	-0.0040	truncata -0.0013	. 0.0022	-0.0077	-0.0025	0.0032	-0.0076	-0.0022	0.0020
2.0	-0.0077	-0.0045	-0.0003	0.0030	£200.0	-0.0188	-0.0144	-0.0112	-0.0057	-0.0031	0.0011	0.0045
7.5	-0.0300	-0.0247	-0.0215	-0.0174	-0.0137	-0.0101	-0.0058	-0.0032	0.0007	0.0033	0.0044	0.0071
3.0	-0.0310	-0.0273	-0.0230	-0.0174	-0.0146	-0.010A	-0.0072	-0.0041	-0.0017	£000.0	0.0040	0.0082
3.5	P.0025	P. 9955	0.0077	0.0110	-0.0477	-0.0466	-0.0378	-0.0348	-0.0337	-0.0284	-0.0230	-0.0184
4.5	9.9030 -0.0170	0.0040	0.0000	0.0100	0.0138	-0.0557	-0.0526	-0.0484	-0.0402	-0.0381	-0.0303	-0.0255
5.0	0.0122	-0.0157 0.0144	-0.0124	-0.0088	-0.0043	-0.0021	0.003%	0.0043	0.0058	0.0113	0.0150	0.6157
	******	*****	-0.0472	-9.0011	-9.0574	-0.0550	-0.0504	-0.041 R	-0.0413	-0.0349	-0.0334	-0.02R2
	R=6 -	PCKC F23	1									
1.5	0.0043	-0.0021	0.0141	0.0044	-0.0014	-0.0071	0.0077	-0.0003	-0.0087	0.0080	0.0004	-0.0066
2.0	0.0054	0.0007	-0.0047	-0.0100	-0.0144	0.0183	0.0134	0.0103	0.0027	-0.000 0	-0.0077	-0.0133
2.5	0.0245	0.0224	0.0174	0.0158	0.0117	9.0074	0.0017	-0.0017	-0.0006	-0.0122	-0.0184	-0.0236 -0.0238
3.0 3.5	0.0243 -0.0107	0.0237	0.0174	0.0147	0.0108	0.0040	0.0055	-0.0027	-0.0051	-0.0074	-0.0144 0.0175	0.0130
4.5	-0.0110	-0.0140 -0.0172	-0.0204 -0.0201	-0.0274 -0.0259	0.0375 -0.0337	0.0364 0.0377	9.0393 5750.0	0.0275 0.0370	0.0263 0.0277	0.0234 0.0300	0.0217	0.0172
4.5	0.0145	0.0117	0.0077	0.0037	-0.0036	-0.0055	-9.0175	-0.0141	-0.0145	-0.0316	-0.0479	-0.0413
5.0	-0.0270	-0.0317	0.0447	0.0427	0.0384	0.0384	0.0341	0.0282	0.0317	0.0255	0.0272	0.0224
		AL			,			•				
			(1-6)!		-0.5) tru							
1.5	-0.0104 -0.0077	-0.0188 -0.0372	-0.0174 -0.0335	-0.0060 -0.0288	-0.0170 -0.0237	-0.0132 -0.0188	-0.0077 -0.0144	-0.0207 -0.0112	-0.0137 -0.0057	-0.0074 -0.0378	-0.0210 -0.0337	-0.0154 -0.0288
7.5	-0.0300	-0.0247	-0.0215	-0.0174	-0.0137	-0.0101	-0.0405	-0.0544	-0.0477	-0.0440	-0.0404	-0.0341
3.0	-0.0310	-0.0273	-0.0230	-0.0174	-0.0140	-0.0100	-0.0042	-0.0753	-0.0714	-0.0477	-0.0413	-0.0534
3.5	-0.0700	-0.0646	-0.0400	-0.0541	-0.0477	-0.0466	-0.0378	-0.0348	-0.0337	-0.0284	-0.0230	-0.0184
4.0	-0.0618	-0.0761	-0.0722	-0.0444	-0.0403	-0.0557	-0.0576	-0.0484	-0.0402	-0.0381	-0.0303	-0.0253
4.5	-0.0170	-0.0157	-0.1344	-0.1278	-9.1208	-0.1147	-0.1054	-0.1037	-0.1007	-0.0EE4	-0.0801	-0.0764
5.0	-0.0811	-0.0742	-0.0372	-0.0644	-0.0374	-0.0550	-9.0504	-0.041R	-0.0413	-0.0349	-0.0334	-0.02R2
	2-6 - 1	KKE rz:	•								-	
1.5	0.00AZ	0.0201	0.0141	0.0044	0.0210	0.0147	0.0077	0.0223	0.0155	0.0000	0.0235	0.0177
7.0	0.0054	P.9353	9.0314	0.0278	0.0232	#.0103	0.0134	0.0103	0.0027	0.0362	0.0315	0.0277
2.5	0.0245	0.0224	0.0174	0.0150	0.0117	0.0074	0.0460	0.0443	0.0402	0.0363	0.0346	0.0314
3.6 3.5	0.0243	0.0237	0.0174	0.0167	0.0108	0.0040	0.0552	0.050R	0.0478	0.04R#	0.0453	0.0403
4.0	0.0491 0.0518	0.0455	0.0434	0.0378	0.0375	0.0344	0.0306	0.0275	0.0283	0.0234	0.0175	0.0130
4.5	0.0310 0.0145	0.0474 0.0117	0.0463 0.0446	0.0454 0.0453	0.0421 0.0424	0.9377	0.0373 0.0572	0.0370 0.05 8 3	0.0297 0.0584	9.0309 9.0524	9.0217 9.0481	0.0172 0.0474
5.0	0.0503	0.0464	0.0447	0.0427	0.0384	0.0384	0.0341	0.0282	0.0312	0.0255	0.0272	0.0224

Table 3. Standard NORMAL approximation risk protection difference (R) between actual ($P[k \le p]$) and stipulated (1- α or β) probabilities of acceptance. Plans in Table 1.

\P1	0.0050	0.0100	0.0150	0.0200	0.0250	0.0700	0.0350	0.0400	0.0450	0.0500	0.0550	0.0400
D	R- PCk		(1-0) (-1- 1-	10.5) tr							
1.5		0.0110	0.0017	0.0047	0.0104		0.0059	0.0109	0.0017	0.0060	0.0077	0.0140
2.0		0.0050	0.0082	0.0112	0.0135	0.0165		0.0210	0.0035	0.0070	0.0072	0.0123
2.5		0.0248	0.0264	0.0037	0.0064	0.0087	0.0122	0.0138	0.016H	0.0187	0.0201	0.0227
3.0		0.0043	0.004	0.0075	0.0120	0.0133	0.0154	0.0187	0.0204	0.0228	6.0242	0.0257
3.5 4.0		0.027E 0.0304	0.0273 0.0317	2020.0	0.031M	0.033 <i>2</i> 0.0357	0.033 7	0.004£ 6.0078	0.0075 0.0070	0.0122	0.0142	9.0154
4.5		0.0236	0.0254	0.0244	0.0280	0.0304	0.0314	0.0327	0.00/0	0.0103 0.0344	0.0222	0.0142 0.0373
5.0	0.0344	0.0376	0.0383	0.0374	0.0071	0.0105	0.0137	0.0160	0.0165	0.0202	0.017#	0.0257
		و د نام و معم										
1.5	R=B - -0:0087	PCk(c' P7	0.0004	-0.0073	-0.0165	0.0011	-0.0070	-0.0166	0.0017			
7.0	0.0017	-0.0030	-0.0003	-0.0137	-0.0177	-0.0257	-0.0338	-0.0387	0.0017	-0.0075 -0.0063	-0.0147 -0.0093	~0.0253 ~0.0156
2.5	-0.0374	-0.0462	-0.0517	0.0013	-0.0021	-0.0057	-0.0136	-0.0157	-0.0230	-0.0281	-0.0278	~0.0387
3.0	-0.0410	0.0027	-0.0004	-0.0054	-0.0076	-0.0117	-0.0151	-0.0244	-0.0270	-0.0357	-0.0384	-0.0436
3.5	-0.0422 -0.0500	-0.0484 -0.0550	-0.0584 -0.0584	-0.0592 -0.0456	-0.0433	-0.0707	-0.0727	0.0074	0.0027	-0.0084	-0.0115	-0.0124
4.5	-0.0300	-0,0330	-0.0336	-0.0359	-0.0480 -0.0378	-0.0812 -0.0517	-0.0858	0.0010	0.0073	0.0014	-0.0034	-0.0034
5.0	-0.0745	-0.0850	-0.0843	-0.07R1	0.0037	3.0038	-0.0564	-0.0415 -0.0070	-0.0735 -0.012 7	-0.0424 -0.0150	~0.0455 -0.0071	-0.0332
									- 0.00.2.	-710207		-010332
		celeta - (c = (c)	truncate							
1.5 7.0	0.0077	0.0021	0.0017	0.0047	-0.0038 -0.0119	0.0015	0.0057	-0.0034	0.0017	0.0040	-0.0051	2000.0
7.5	-0.0054	-0.0020	0.0007	0.0037	0.0064	-0.0077 0.0087	-0.0033 0.0122	-0.0007	0.0035	0.0070	0.0072	0.0173
3.0	0.0015	0.0043	9.0048	0.0075	0.0120	0.0133	0.0122	0.013R 0.0187	0.014R 0.0204	-0.015# -0.0182	-0.0138 -0.0157	-0.0089 -0.0124
3.5	-0.0142	-0.0107	-0.0077	-0.0048	-0.0024	0.0007	0.0023	0.0044	0.0075	0.0122	0.0142	9.0154
1.0	-0.0132	-0.0102	-0.0076	-0.0045	-0.0024	0.0017	0.0040	0.007#	0.0070	. 0.0103	0.0130	0.0142
4.5 5.0	0.0220 -0.0014	0.0236 0.0014	0.0254 0.0031	0.0066	-0.0264 0.0071	-0.0205	-0.0173	-0.0143	-0.0074	-0.0106	-0.0084	-0.0024
		010074	0.0031	0.0000	0.0071	0.0105	0.0137	0.0160	0.0195	0.0202	0.0178	0.92 57
	R-B -	PCK(cl+2)										
1.5	-0 . 0087	0.0077	0.0004	-0.0073	0.0067	0.0011	-0.0070	0.0084	0.0017	-0.0075	0.0073	0.0017
7.0	0.0017	-0.0020	-0.0063	-0.0139	0.0177	0.013H	0.0077	0.0064	0.0002	-0.0063	-0.0073	-0.0154
2.5 3.0	0.0141 0.0048	0.0077 0.0027	0.0041 -0.0004	0.0013 -0.0054	-0.0021 -0.0078	-0.0057	-0.0134	-0.0157	-0.0230	0.0261	0.0757	0.0175
3.5	0.0240	0.0027	0.0178	0.0148	0.0146	-0.0112 0.0105	-0.0151 0.0077	-0.0246 0.0074	-0.0270 0.0027	0.0273 -0.0084	0.0280 -0.0115	0.0253 -0.0124
4.0	0.0257	0.0234	0.0217	0.0181	0.0173	0.0101	0.0080	0.0010	0.0073	0.0014	-0.0034	-0.0034
4.5	-0.0247	-0.02R4	-0.0338	0.0407	0.0372	0.0335	0.0314	0.0274	0.0237	0.0304	0.0274	0.0213
5.0	0.0147	0.0128	0.0128	0.0046	0.0037	0.0038	-0.0033	-0.0070	-0.0127	-6.0150	-0.0071	-0.0332
	B= 255.6	:* +13 - (11-411	e'n (c -	0.5) Lru							
1.5	-0.0074	-0.0021	-0.0151		-0.0038	-0.0154	-0.00/7	-0.0034	-0.0158	-0.0100	-0.0051	0.000X
2.0	-0.0283	-0.0243	-0.0176		-0.0117	-0.0077	-0.0033	-0.0007	-0.0267	-0.0233	-0.0204	-0.0157
2.5	-0.0034	-0.0020	0.0007		-0.0345	-0.032R	-0.0247	-0.0244	-0.0174	-0.0156	-0.0138	-0.00RT
2.0	0.0015 -0.0142	-0.0515 -0.0107	-0.0474		-0.0362	-0.0339	-0.0322	-0.0257	-0.0224	-0.0182	-0.0157	-0.0124
3.5 4.0		-0.0102			-0.0024 -0.0024	0.0007 0.0019	0.0023 0.0040	-0.0485 -0.0747	-0.0430 -0.0770	-0.0534 -0.0704	-0.0498 -0.0447	-0.0472 -0.0425
4.5							-0.0173		-0.0074	-0.0106	-6.0064	-0.0024
5.0	-0.0014	0.0014	0.0031			-0.0681	-0.0806		-0.0477	-0.0637	-0.0477	-0.0521
		تدام بيس		•								
1.5	7- B P	[k(c"]r2] 0.007 7	0.0201	0.015R	0.00R2	0.0231	0.0145					
2.0	0.0353	0.0318	0.0201	0.0242	0.0177	0.015H	0.0077	0.0084	0.0242 0.0337	0.0145 0.0314	0.0093 0.0274	0.0017 0.0251
2.5	0.0141	0.0077	0.0041	0.0438	0.0418	0.0377	0.0348	0.0337	0.0271	0.0241	0.0252	0.0175
3.0	0.0068	0.0502	0.0464	0.0457	0.0433	0.0428	0.0408	0.0354	0.0330	0.0273	0.0280	0.0253
3.5 4.0	0.0240 0.025 7	0.0224	0.0178	0.0168	0.0144	0.0105	0.0077	0.0574	0.0574	0.0521	0.0507	0.0507
4.5	0.0257 0.0451	0.0234 0.0437	0.0217 0.0413	0.0181 0.0407	0.0173 0.0372	0.0335	0.0080 0.0314	0.0604 0.0276	0.0437 0.0239	0.0413	0.0574	0.0578
5.0	0.0147	0.0128	0.0120		0.0458	0.0442	0.0637	0.0424	0.0237	0.0304 0.0402	0.0274 0.0440	0.0213 0.0538

Table 4. ARCSINE transformation risk protection difference (R) between actual $(P[k \le c \mid p])$ and stipulated $(1-\alpha \text{ or } \beta)$ probabilities of acceptance. Plans in Table 1.

against Type I error may be as large as 14%. When <u>c'</u> is adopted, protection against Type I error is usually attained, or is at most 1.25% below the stipulated producer's risk probability, but under-protection against Type II error may be as large as 10%. When no continuity correction is used with <u>c</u>, there is no consistent risk protection, and under-protection against either type of error may be as large as 6%.

Arcsin Transformation

As evidenced in Table 5, acceptance control plans obtained from the arcsin transformation consistently provide one-tail protection. When $\underline{c^*}$ is used, protection against Type II error is attained, but not against Type I error. Under-protection against Type I error may be as large as 9%. When $\underline{c^*}$ is adopted, protection against Type I error is attained, but under-protection against Type II error may be as large as 10%. When no continuity correction is used with \underline{c} , no consistent protection is attained, and under-protection against either type of error may be as large as 3%.

SIMULATION STUDY

A computer program simulating item manufacture and control charts, written by Davis (1977), was used to analyze the performance of ACC's derived from the binomial distribution, standard normal approximation, and arcsin transformation. Twenty replications of this simulated process were made, using common random numbers for variance reduction.

Process Description

It is desired to have producer and consumer risks of 5% and 10%, respectively. The cost of a Type I error is considered to be greater than that of a Type II error in this simulation; thus, $\underline{c'}$ is used with the

Table 5. BINOMIAL ACC Plan Simulation Results.

SUB GROUP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	NONCON- FORMANCES 3 2 0 4 0 5 1 2 3 4 5 2 2 4 4 5	SUB GROUP 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36	NONCON- FORMANCES 3 2 4 3 3 2 3 2 3 1 1 1 1	SUB GROUP 41 42 43 44 45 46 47 - 48 49 50 51 52 53 54 55 56	NONCON- FORMANCES 4 3 2 3 1 3 5 5 3 1 12 8 8 6 13 8
17			1 3 2		
18 19 20	2 3 7	39 40	2	59 60	10

approximations because of its increased Type I error protection. In Table 1, when an APL of 1.5% and a discrimination ratio, \underline{D} , of 3.5 are chosen (i.e., RPL = 5.25%), the acceptance control plans are as follows:

Method	<u> </u>	<u> </u>	<u>c'</u>	<u>c*</u>	Plan Chosen
BINOMIAL ARCSIN	175.0 182.0	5.00 6.73	7	6	(175, 5) (182, 7)
NORMAL	168.0	5.11	5	4	(168, 5)

Thus the Acceptance Control Limits were positioned at 5.5 for the binomial and standard normal approximation and at 7.5 for the normalized arcsin transformation. The simulation "manufactured" 10,500 items. Initially the manufacturing process had a nonconforming percentage of 1.5, the AQL. After the 8,750th item produced, the process shifted to 5.25% nonconforming, the RQL level. Thus there was a shift from the expected acceptable process level to the rejectable process level to test the plans at the stipulated extremes.

Control Chart Analysis

The control charts in Figures 3 and 4 show the number of nonconforming units found in each subgroup of the three acceptance plans. Tables 5, 6, and 7 contain the simulated data used to plot these Figures. The process shifted to the RPL after the 50th subgroup for the exact binomial plan, and in the middle of the 49th and 53rd subgroups for the arcsin transformation and normal approximation plans, respectively.

The binomial plan made one Type I error (subgroup 20) in 50 subgroups of good quality and no Type II errors were made in the final 10 subgroups. The arcsin transformation plan made one Type I error (subgroup 32) out of 48 good quality subgroups and no Type II errors in the last ten subgroups. The standard normal approximation plan made no Type I errors in the first 52

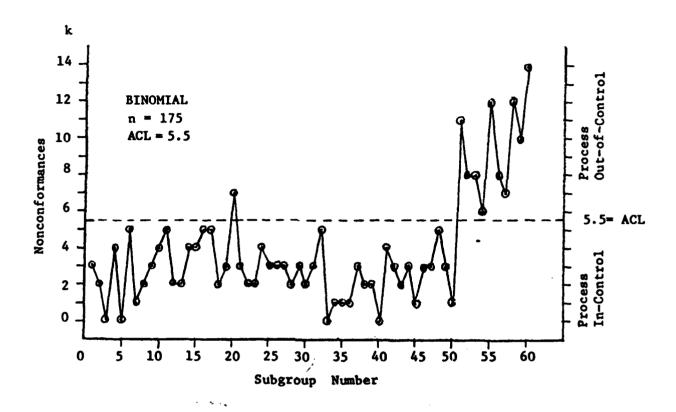


Figure 3. Acceptance Control Chart, Exact Binomial

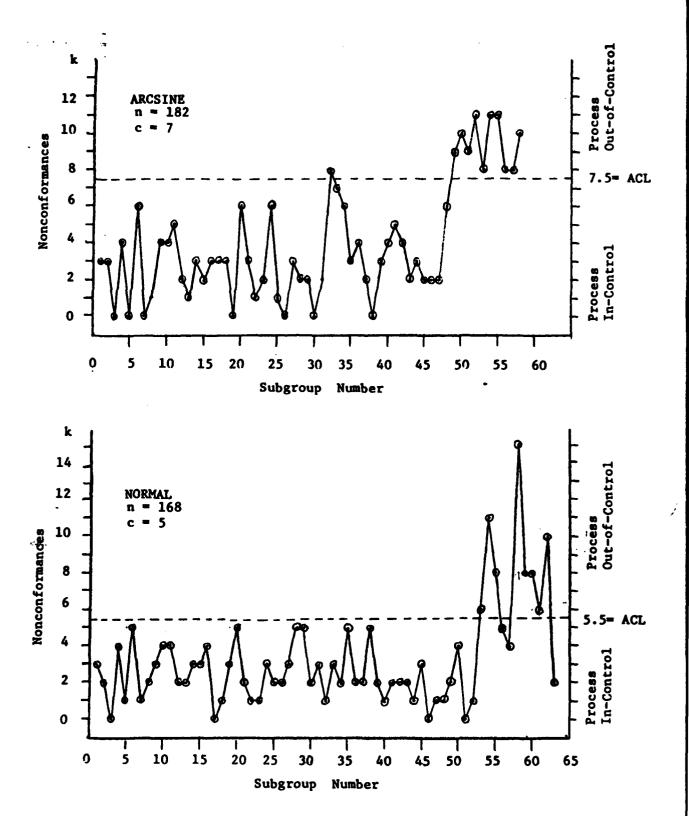


Figure 4. Acceptance Control Charts for ARCSIN and NORMAL approximations.

Table 6. ARCSINE ACC Plan Simulation Results.

SUB GROUP	NONCON-	SUB	NONCON-	SUB	NONCON-
OKUUP	FORMANCES	GROUP	FORMANCES	GROUP	FORMANCES
j	3 3	21	3	41	5
2	3	22	1	42	4
3	0	23	2	43	2
4	3	24	6	44	3
5	0	25	1	45	2
6	6	26	0	46	2
7	0	27	3	47	2
8	1	28	2	48	6
9	4	29	2	49	9
10	4	30	0	50	10
11	5	31	2	51	ğ
12	2	32	8	52	11
13	1	33	7	53	8
14	3	34	6	54	12
15	2	35	3	55	12
16	3	36	4	56	8
17	3	37	2	57	8
18	3	38	0	58	10
19	0	39	3		
20	6	40	4		

Table 7. NORMAL ACC Plan Simulation Results.

SUB GROUP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	NONCON- FORMANCES 3 2 0 4 1 5 1 2 3 4 2 2 3 4 0 1 3 5	SUB GROUP 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38	NONCON- FORMANCES 2 1 3 2 3 5 2 3 1 3 2 5 2 1 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SUB GROUP 41 42 43 44 45 46 47 48 49 50 51 55 57 58 59 60	NONCON- FORMANCES 2 2 2 1 3 0 1 1 2 4 0 1 6 11 8 15 5 4 8
20	5	40	1.	60 61 62 63	6 10 3

subgroups, but had three Type II errors (subgroups 57, 58 and 60) in the last eleven subgroups, when the process had shifted to the RPL.

The total number rejected in a subgroup may be expected to exceed the ACL for either of two reasons, (1) the existence of assignable causes, or (2) the existence of a quality level which exceeds the APL. In either case, the only clue given by the acceptance control chart as to the cause of lack of control is the time at which lack of control at the desired level was observed. For this reason, immediate corrective action should be taken whenever a point exceeds the ACL. This simulation did not include such corrective action because it was desired to observe the consistency of each control chart in providing the desired risk protections.

CONCLUSIONS

Three methods for obtaining subgroup sizes and acceptance control limits were compared. In addition to utilizing the exact binomial distribution, the standard normal approximation and a normalized arcsin transformation were used. Acceptance plans obtained by using the binomial distribution provide the stipulated risk protections (guaranteed over protection) for both producer and consumer. This results from the strict application of the inequality constraints of equations (3) and (4). When a continuity correction of 0.5 is added to (subtracted from) the <u>c</u> derived from either of the latter two approximation methods, strict risk protection against Type I (Type II) error is attained, but not against both error types. If no continuity correction is used, the risk protection from these approximations is inconsistent; i.e., risk protection alternates against both types of errors, with no discernable pattern.

For the risk levels studied ($1-\alpha=0.95$ and $\beta=0.10$) and the wide range of values of $\underline{p_1}$ and $\underline{0}$ studied, the normalized arcsin transformation yielded results closer to design than did the standard normal approximation. Risk protection losses ranged as high as 2.96% for the producer ($1-\alpha$) and 3.38% for the consumer (β) with no continuity correction factor applied. These are the maximum (underlined) negative numbers in Table 4. With a continuity correction factor of 0.5 added to the solving value of \underline{c} , the producer received at least the required protection but the consumer loss of protection reached as high as 9.81% (nearly doubled). With 0.5 subtracted from the solving value of \underline{c} , consumer protection at the specified level was assured but loss of producer protection increased to 9.08%, i.e., from a design level of 0.05 to as high as 0.1408. Unless protection at one level is vital, as opposed to protection at the other level, no continuity correction is recommended when the arcsin transformation is to be used.

Results from the standard normal approximation were not as good, in general, as those achieved by applying the arcsin transformation. Without adjustment by a continuity correction factor, loss of producer protection ranged as high as 6.92% and loss of consumer protection as high as 4.29% (negative underlined values in Table 3). With 0.5 added to the solving value of c, loss of producer protection was reduced to 1.2% but loss of consumer protection was increased markedly to 10.19%. With 0.5 subtracted from the solving value of c, loss of producer protection increased to 13.64% but consumer protection at the design level was assured. As was the case with the normalized arcsin transformation, no continuity correction can be recommended unless it is imperative to meet (or nearly meet) the design level of protection at either the producer or the consumer quality protection level.

Both the standard normal and arcsin transformation require the evaluation of only two equations to obtain an ACC plan $(\underline{n},\underline{c})$ pair. These equations easily may be evaluated using Standard Mathematical Tables or a scientific calculator, since they only require the use of square root, sine, and inverse sine functions. The binomial distribution requires at least \underline{c}^2 evaluations of equation 2, which contains factorial and exponential terms, and a search for the minimum \underline{n} among various $(\underline{n},\underline{c})$ pairs that satisfy the inequalities in equations 3 and 4. However, even most home computers have the capability of performing these evaluation and search tasks quickly; they would be tedious and time consuming if performed using tables and/or pocket calculators.

Finally, to assure the desired protection for both producer and consumer, the exact binomial should be used to obtain ACC plans, provided computer facilities are available. The normalized arcsin transformation is preferable to the standard normal approximation because its likely degree of under-protection is about half that of the standard normal. Possible under-protection afforded by the standard normal is about double that of the arcsin in absolute terms.

A complete listing of the computer programs used to develop and evaluate the various plans is provided in the Appendix.

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APPENDIX

```
20 REM* PROGRAM: BINOMIAL ACCEPTANCE CONTROL PLAN (N+C)
40 DIM SUMLOG(1000)
50 NMAX = 1
60 \text{ SUMLOG(NMAX)} = 0
70 INPUT "ENTER PRODUCER & CONSUMER'S RISKS ", A,B
80 INPUT "ENTER ACCEPTABLE & REJECTABLE PROCESS LEVELS ", P1,P2
90 GOSUB 130
    PRINT "SUBGROUP SIZE N = ";N
    FRINT *CONTROL LIMIT C = *$C
110
120 END
140 REM#
         SUBROUTINE: SINGLE SAMPLING PLAN SEARCH
150 REM#
160 REMX
         REFERENCE:
                    GUENTHER (1969) & HAILEY (1980)
170 REM*
180 REM#
         GIVEN:
                      PRODUCER'S RISK
                A
190 REM*
                В
                      CONSUMER'S RISK
200 REM*
                P1 =
                      ACCEPTABLE QUALITY LEVEL (ARL)
210 REM#
                      REJECTABLE QUALITY LEVEL (RQL)
220 REM#
230 REM*
                      MINIMUM SUBGROUP SIZE
        FINDS:
                N
240 REM#
                  =
                      NONCONFORMANCE CONTROL LIMIT
                C
260 N = 1
270 \text{ C} = -1
280 C = C + 1
290 P = P2
300 N = N + 1
310 GOSUB 370
                        N REM*** CALL BINOMIAL (P2, N, C, PACC)
320
     IF PACC > B THEN 300
     P = P1
330
340 GOSUB 370
                        N REM*** CALL BINOMIAL (P1, N, C, PACC)
350
     IF PACC < (1-A) THEN 280
360 RETURN
380 REM*
        SUBROUTINE: CUMULATIVE BINOMIAL PROBABILITY
390 REM*
                     SUBGROUP SIZE
400 REM*
        GIVEN:
               N
                 ===
                     NONCONFORMANCE CONTROL LIMIT
410 REMX
               C
                  ===
                     PROBABILITY OF NONCONFORMANCE
420 REM#
430 REM#
440 REM* FINDS: PACC ≈
                       PROBABILITY OF ACCEPTANCE (CUM. BINOMIAL)
460 Q = 1-P
470 CUMULA = 0°N
480 \text{ IF C} = 0 \text{ THEN } 600
490 IF N <= NMAX THEN 540
                        N REM*** LOG SUMS ALREADY IN MEMORY
500 \text{ FOR } K = (\text{NMAX+1}) \text{ TO N}
                      N REM*** COMPUTE ONLY NEW LOG SUMS
510
       SUMLOG(K) = LOGIO(K) + SUMLOG(K-1)
520 NEXT K
530 \text{ NMAX} = N
                     N REM*** LARGEST LOG SUM (FACTORIAL) IN MEMORY
540 \text{ PLOG} = L0G10(P)
550 \text{ QLOG} = \text{LOGIO(Q)}
                     N REM*** COMPUTE CUMULATIVE PROBABILITY
560 FOR K = 1 TO C
       FACTOR = SUMLOG(N) - SUMLOG(N-K) - SUMLOG(K)
570
580
       CUMULA = 10^{\circ}(FACTOR + K*PLOG + (N-K)*QLOG) + CUMULA
590 NEXT K
600 PACC = CUMULA
610 RETURN
```

```
CC----
       CC
             PROGRAM: COMPARES SINGLE SAMPLING PLANS FOR A PROCESS
       CC
                       WHICH HAS BINOMIALLY DISTRIBUTED DEFECTIVES.
       CC
      CC
             PROGRAMMER: CARLOS AMADO
                                                             FALL '81
      CC
       CC
             RESEARCH FOR: DR. R.L. LEAVENWORTH, ISE DEPT, UNIV. OF FLORIDA
       CC---
0001
             DIMENSION CLU(2); CLL(2)
0002
             CALL ASSIGN (2, 'SINGLE, DAT') ! OUTPUT FILE
0003
             CALL PUTCHR (26,5) ! CLEAR CRT SCREEN
        130
0004
             WRITE (5,131)
0005
        131
             FORMAT ('OENTER DATA (START IN 1ST LETTER OF TITLE)'//
                                AL.FA
                                        P1
                                                BETA
            I
                     ' PO
                                                         ITER81)
0006
             READ (5,133,ERR=130) PO, ALFA, P1, BETA, ETER8
0007
        133
             FORMAT (5(F7.4,1X))
8000
             IF (PO.LE.O) GO TO 199
0010
             IF (PO.EQ.P1) 60 TO 127
             IF (ETER8.NE.O) GO TO 126
0012
0014
             GO TO 129
0015
       127
             URITE (5,*)
             WRITE (5,*) 'PO CAN NOT EQUAL P1 (ZERO DIVIDE ERROR)'
0016
0017
             GO TO 194
             CALL ITERS (ALFA; PO; BETA; P1; A; ETERS)
0018
       126
             IF (A.ER.'Y') GO TO 196
0019
0021
             IF (A.EQ.'R') GO TO 194
0023
             60 TO 130
0024
       129
            WRITE (2:128) PO: ALFA: P1: BETA
0025
            FORMAT (///' GIVEN (PO, A, P1, B):',4(F7.4:2X))
       128
0026
             CALL ARCSIN (ALFA, PO, BETA, P1, SN, C, CLU, CLL)
0027
             WRITE (5,*) SN, C, ' FROM ARCSINE'
0028
            WRITE (2:*) ' '
0029
            WRITE (2,*) 'ARCSINE TRANSFORMATION'
0030
            M= 1
0031
            GO TO 134
0032
       132
            CALL NORMBI (ALFA, PO, BETA, P1, SN, C, CLU, CLL)
0033
            WRITE (2,*) /
0034
            WRITE (2,*) 'NORMAL APPROXIMATION'
0035
            M= 2
0036
            GO TO 134
0037
       136
            CALL GUNTHR (ALFA, PO, BETA, P1, SN, C)
0038
            WRITE (2,*) / /
0039
            WRITE (2:*) 'EXACT BINOMIAL'
0040
            M= 3
0041
       134
            IF (C.EQ.999.) 60 TO 199
0043
            CALL EXACT (SN;PO;C;BXLEC;N)
0044
            CALL EXACT (SN,P1,C,P,N)
      C
```

.

```
WRITE (2:135) SN: BXLEC: C: P
0045
0046
       135 FORMAT ('SINGLE SAMPLING PLAN: //
                    ' SAMPLE SIZE =',F9.2,5X,
                    ' P > 1-A =',F9.4/
           Ι
                    / MAX DEFECTS ==/yF9.2,5X;
                    ' P < B = ='rF9.4)
0047
            GO TO (132,136,130), M
0048
       194 URITE (5,*)
0049
            WRITE (5:*)' INPUT ERROR! TYPE "R" TO RESTART'
0050
       196
            READ (5,197) A
0051
       197
            FORMAT (A1)
0052
            IF (A.EQ.'R'.OR.A.EQ.'N') GO TO 130
0054
       199
            WRITE (5,*)
0055
            STOP '
                     HAVE A GOOD LIFE'
            END
0056
```

```
SUBROUTINE GUNTHR (ALFA, PO, BETA, P1, SN, C)
0001
      00
            PROGRAM: OBTAINS EXACT BINOMIAL SINGLE SAMPLING PLAN
      CC
            REF: GUENTHER: W.C., "USE OF BINOMIAL, HYPERGEOMETRIC: AND
      CC
                     POISSON TABLES TO OBTAIN SAMPLING PLANS*, JOURNAL OF
                     QUALITY TECH: VOL 1: NO. 2: APRIL 1969: PP 105-109.
      CC
      CC---
            C= -1. ! START AT C=0
SNS= 1. ! START AT SNS=2
0002
      1
0003
      C
0004
            C= C+ 1.
0005
      - 3
            SNS= SNS+ 1.
            CALL EXACT (SNS, P1, C, BXLEC, N)
0006
0007
            (F (BXLEC.GY.BETA) GO TO 3
0009
            SNL = SNS- 1. ! SMALLER SNL NOT NEEDED
0010
            SNL= SNL+ 1.
      C
            WRITE (5:*) SNS: C: SNL: BXLEC
0011
            CALL EXACT (SNL, PO, C, BXLEC, N)
0012
0013
            IF (BXLEC.GE.(1.-ALFA)) GO TO 4
            SNL = SNL - 1. ! PREVIOUS SNL IS THE ONE WANTED
0015
            IF (SNS.GT.SNL) 60 TO 2
0016
0018
            SN= SNS
0019
            RETURN
0020
            END
```

```
0001
             SUBROUTINE EXACT (SN, P, C, BXLEC, N)
       CC--
       CC
             PROGRAM: COMPUTES EXACT CUMM. BINOMIAL PROBABILITY OF X.LE.C
       CC
       CC
             METHOD:
       CC
                        "N" NUMBER OF LOG(10) SUMS ARE COMPUTED ONCE, ONLY,
       CC
                        AND STORED IN "SUMLOG(I)" VECTOR.
       CC
                     B. 10**( SUMLOG(I) ) REPRESENTS I-FACTORIAL; THEREFORE,
       CC
                        FACTORIAL MULTIPLICATIONS ARE REDUCED TO SUMMATIONS.
       CC
                        ALL FACTORIALS NEEDED ARE IN STORAGE UP TO SUMLOGIN)
       CC
                     C. WHENEVER ITERATIONS ARE RUN, THE SUMLOG(I)'S IN MEMOR
       CC
                        ARE NOT RECOMPUTED.
       CC
                     D_{\star} N > C > Of N-FAC > C-FAC; AND SUMLOG(N) > SUMLOG(C).
       CC
                     E. SUMLOG(I) SUBTRACTION = I-FACTORIAL DIVISION.
       CC
                     F. LOG(10) ALLOWS EFFICIENT HANDLING OF LARGE NUMBERS.
       CC
       CC
                           CARLOS H. AMADO, ISE DEPT., UNIV. OF FLORIDA
             PROGRAMMER:
       CC-
       CC
             GIVEN:
                        SN
                               SAMPLE NUMBER (SIZE)
       CC
                               = PROB. OF DEFECTIVES
       CC
                        C
                               = # OF DEFECTIVES IN SAMPLE
       CC
       CC
             COMPUTES: BXLEC = BINOMIAL PROB (X.LE.C)
       CC
                        SUMLOG(I) = VECTOR CONTAINING SUM OF LOG(1) THRU LOG
       CC-
0002
             VIRTUAL SUMLOG(9000)
0003
             D = 1.-P
0004
             NN = SN
      C
      r:
             >>> BINOMIAL PROB. WHEN C=0 <<<
0005
             CSUMS = Q **NN
0006
             IF (C.EQ.O.) 60 TO 333
      C
      C
             >>> AVOID RECOMPUTING SUMLOG(I)'S ALREADY IN MEMORY <<<
      C
8000
             IF (NN.GT.9000) 60 TO 998
IF (N-NN) 100,211,211
0010
0011
      100
             M: N+ 1
      C
      C
             >>> COMPUTE N SUMLOGS --EQUIVALLENT TO N-FACTORIAL <<<
      C
0012
             TF (M.GT.1) GO TO 110
0014
             SUMLOG(1) = 0.
0015
             M = 2
0016
       110
             DO 111 I= Mr NN
0017
                    SUMLOG(I) = ALOG1O(FLOAT(I)) + SUMLOG(I-1)
0018
       111
             CONTINUE
      C
             >>> COMPUTE C CSUMS --EQUIVALLENT TO SUM OF PROB COMBINATIONS
      C
                 I.E., CUMMULATIVE BINOMIAL DISTRIBUTION COMPUTATION
0019
       211
             KC = C
0020
             N::: NN
      C
```

```
SINGLE, SINGLE/LI:1=SINGLE
```

```
C
             >>> SUM (ACCUMULATE) PROBABILITIES <<<
      C
\frac{0021}{0022}
             PLOG= ALOG10(P)
RLOG= ALOG10(Q)
0023
             00 322 K= 1, KC
0024
                     CSUMS = 10.**(SUMLOG(N) - SUMLOG(N-K) - SUMLOG(K)
                                          +K*PLOG +(N-K)*RLOG > +CSUMS
0025
       322
             CONTINUE
0026
       333
             BXLEC= CSUMS
0027
             RETURN
0028
       998
             WRITE (5,999) SN, P, C
0029
       999
             FORMAT ('OWHOOPS!!! SAMPLE SIZE =';F10.2//
                      ' AT P =',F10.4,' AND C =', F10.4)
0030
             STOP
0031
             END
```

```
SUBROUTINE NORMBI (ALFA, PO, BETA, P1, SN, C, CLU, CLL)
0001
      CC---
                       COMPUTES A SINGLE SAMPLING PLAN USING THE
      CC
            PROGRAM:
                       NORMAL APPROXIMATION FOR A BINOMIAL DISTRIBUTION
      CC
      CC
      CC-
0002
            DIMENSION CLU(2), CLL(2), ZV(12), ZT(12), Z(2)
0003
            DATA ZU(1)/2.326/, ZU(2)/2.054/, ZU(3)/1.881/, ZU(4)/1.751/,
                  ZV(5)/1.645/, ZV(6)/1.555/, ZV(7)/1.474/, ZV(8)/1.405/,
                  ZV(9)/1.34/, ZV(10)/1.282/, ZV(11)/1.036/, ZV(12)/.842/
0004
            DO 29 I= 1, 10
0005
       29
                   ZT(I) = 1.- I/100.
0006
            ZT(11) = .85
0007
            ZT(12) = .80
8000
            P2: 1.-ALFA
            K= 1
0009
0010
            no 31 I= 1, 12
       30
                   IF (PZ.NF.ZT(I)) GO TO 31
0011
0013
                   Z(K) = ZV(I)
                   60 TO (32;33); K
0014
0015
       31
            CONTINUE
            WRITE (5:*) 'ERROR' ALFA OR BETA NOT IN DATA STATEMENT'
0016
            C= 999.
0017
0018
            RETURN
0019
       32
            PZ= 1.-BETA
            K= 2
0030
            GO TO 30
0021
            PQ0= (1- P0)* P0
PQ1= (1- P1)* P1
0022
       33
0023
             SN= ((Z(1)*SQRT(PQ0) + Z(2)*SQRT(PQ1))/(P1-P0))**2
0024
            C= Z(1)* SQRT(SN*PQO)+ SN* PO
0025
      C
             RETURN
0026
0027
            END
```

```
0001
             SUBROUTINE ARCSIN (ALFA, PO, BETA, P1, SN, C)
       CC--
       CC
                        SINGLE SAMPLING PLAN USING AN ARCSINE NORMALIZING
       CC
                        TRANSFORMATION* TO APPROXIMATE A BINOMIAL PROCESS.
       CC
       CC
                                                       ARCSINE TRANSFORMATION
                            NORMAL
       CC
                        2.
                            FREEMAN & TUCKEY (F & T)
       CC
       \mathbf{cc}
             REF:
                    JOHNSON, N. S. KOTZ, DIST. IN STATISTICS -DISCRETE DIST. 4
       CC
                        HOUGHTON MIFFLIN CO, BOSTON, 1969, P 65.
       CC
                              - PRODUCER'S RISK PROBABILITY OF REJECTION
       CC
             GIVEN:
                        ALFA
                              = CONSUMER'S
                                                                  ACCEPTANCE
       cc
                        BETA
                        PO
                              # ACCEPTABLE PROCESS LEVEL
       CC
       CC
                        P1

    REJECTABLE

       CC
       CC
             COMPUTES: SN
                              ■ SAMPLE SIZE
                              ■ MAX NUMBER OF DEFECTIVES IN ACCEPTANCE
       CC
                        C
       CC
       CC
             VARIABLES:
       CC
                        7(1)
                                # 7(1-ALFA)
       CC
                        7(2)
                                = Z(1-BETA)
                        SINV(1) = ARCSINE OF SQRT(1-ALFA)
       CC
                        SINV(2) =
                                                  (1-BETA)
       CC
                                = SAMPLE SIZE OF NORMAL ARCSINE TRANSFORMATIO
       CC
                        SS(1)
                                           .
       CC
                        88(2)
                                =
                                                  F & T
                                - ACCEPTABLE # DEFECTIVES IN NORMAL
       CC
                        D(1)
                                = ACCEPTABLE * DEFECTIVES IN F % T
      CC
                        \mathfrak{D}(2)
0002
             DIMENSION Z(2), SINV(2), SS(2), D(2), ZT(12), ZV(12), P(2)
0003
             DATA ZV(1)/2.326/, ZV(2)/2.054/, ZV(3)/1.881/, ZV(4)/1.751/,
            T
                  ZV(5)/1.645/, ZV(6)/1.555/, ZV(7)/1.474/, ZV(8)/1.405/,
            I
                  ZV(9)/1.34/; ZV(10)/1.282/; ZV(11)/1.036/; ZV(12)/.842/
0004
             DO 29 Im 1, 10
0005
       29
                   ZT(I) = 1.- I/100.
0006
             ZT(11)= .85
             2T(12) = .80
0007
0008
             P(1)= P()
0009
             P(2)= P1
      C
0010
            PZ= 1.- OLFA
0011
            K= 1
0012
       30
            DO 31 I= 1, 12
0013
                   IF (PZ.NE.ZT(X)) GO TO 31
0015
                   7(K)= 7U(I)
0016
                   SORPH SORT(P(K))
0017
                   SINV(K)= ATAN( SQRF/ SQRT(-SQRP*SQRF+1) ) ! ARCSIN
0018
                   60 TO (32,33), K
            CONTINUE
0019
       31
0020
            WRITE (5,*) 'ERROR: ALFA OR BETA NOT IN DATA STATEMENT'
0021
            C= 999.
            RETURN
0022
0023
       32
            PZ= 1.-BETA
```

```
CONTINUE AV
SINGLE, SINGLEZLI: 1=SINGLE
0024
            K=2
            GO TO 30
0025
      C
33
0026
            SS(2) = ( (Z(1)+Z(2))/ (SINV(2)-SINV(1)) )**2
0027
            SS(1)= SS(2) /4
0028
            X = SINV(1) + Z(1) / (2*SQRT(SS(1)))
0029
            D(1)=(SS(1)+0.75)*(SIN(X)**2)-(3.78.)
      C
0030
            SN= SS(1)
0031
            C= D(1)
0032
            RETURN
0033
            END
```

.

```
0001
             SUBROUTINE ITERS (ALFA, PO, BETA, P1, A, ETERS)
       CC---
       CC
             PROGRAM:
                       DETERMINES SEVERAL SINGLE SAMPLING PLANS
       CC
                       BY CHANGING PARAMETER VALUES IN EACH ITERATION.
       CC----
0002
             DIMENSION SS(3), CC(3), BO(3), B1(3)
0003
             COMMON /ETER/ AL:AS:AH:BL:BS:BH:POL:POS:POH:P1L:P1S:P1H
0004
             WRITE (5:101)
0005
        101
            FORMAT ('OENTER ITERATION (STEP) AND HIGHEST VALUES'//
                      (ALFA) ALFA (PO)
                                           F()
                                                   (P1)
                                                                  (BETA) BETA'
                                                          P1
0006
             READ (5:103) AS: AH: POS: POH: PIS: PIH: BS: BH
0007
       103
             FORMAT (8F7.4)
0008
             IF (AS.LT.O.OR.AH.LT.ALFA) GO TO 194
0010
             IF (BS.GT.O) GO TO 104
0012
             BS= AS
0013
             BH= AH
0014
       104
             IF (POS.LT.O.OR.POH.LT.PO.OR.P1S.LT.O.OR.P1H.LT.P1.OR.
            7
                 Pis.LT.Pos.OR.BH.LT.BETA) GO TO 194
0016
             AL. AL.FA
0017
             BL = BETA
             POL= PO
0018
0019
             P11.= P1
0020
             IF (ETFR8.EQ.8.) GO TO 114
             GO TO 110 ! BEGIN ITERATIONS
0022
0023
       106
            P1= P1+ P1S
0024
             IF (P1.LE.P1H) GO TO 110
0026
             P1= P11
0027
             PO= PO+ POS
0028
             IF (PO.LE.POH) GO TO 110
0030
             PO= POL
0031
             ALFA= ALFA+ AS
0032
             IF (ALFA-LE-AH) GO TO 110
0034
             ALFO= AL
0035
             BETA- BETA+ BS
0036
             IF (BETA-LE-BH) GO TO 110
0038
            WRITE (5,*)
            WRITE (5,*)' END OF ITERATIONS! END SESSION?
0039
            A= 'Y'
0040
0041
            RETURN
0042
       194
            A='R'
0043
            RETURN
0044
       110
            CALL ARCSIN (ALFA, PO, BETA, P1, SS(1), CC(1))
0045
            CALL NORMBI (ALFA, PO, BETA, P1, SS(2), CC(2))
0046
            CALL GUNTHR (ALFA, PO, BETA, P1: SS(3); CC(3))
0047
            no 112 I= 1, 3
                    CALL EXACT (SS(I), PO, CC(I), BO(I), N)
0048
0049
       112
                    CALL EXACT (SS(I), P1, CC(I), B1(I), N)
0050
            A1= 1.-ALFA
            WRITE (2:113) A1, BETA, PO, P1, SS(3), CC(3), BO(3), B1(3),
0051
                  $$(1), CC(1), BO(1), B1(1), $$(2), CC(2), BO(2), B1(2)
```

```
SINGLE, SINGLE/LI:1=SINGLE
       113 FORMAT ('OGIVEN (1-A, B, PO, P1):',4(F7.4;',')//
0052
                                                          P>1-A
                                                                    P<81/
                   ' SINGLE SAMPLING PLAN: N'+7X+'C
           7.
           7.
7.
                   ' EXACT BINOMIAL',8X,2F8,2,2F8,4/
                   ' ARCSINE TRANSFORMATION',2F8.2,2F8.4/
                   ' NORMAL APPROXIMATION ',2F8.2,2F8.4)
           7.
0053
            GO TO 106
0054
       114 CALL ITER88 (ALFA: PO: RETA: P1: A)
0055
            RETURN
            END
0056
```

.

```
0001
            SUBROUTINE ITER88 (ALFA, PO, BETA, P1, A)
      COMPARES DESCRIMINATION RATIOS (P1/P0)
      0002
            DIMENSION SS(9); CC(9); BO(9); B1(9); PA(3); PR(3)
0003
            COMMON /FTER/ ALFAS, AH, BL, BS, BH, POL, POS, POH, P1L, P1S, P1H
0004
       112
            WRITE (5:*)
            WRITE (5:*)'ENTER D-STEP FOR P1'
0005
0006
            READ (5**) DS
0007
            JF (DS.LT.0) GO TO 112
      C
0009
       114
            A1m 1.-ALFA
0010
            WRITE (2:115) Al;ALFA;BETA
0011
            WRITE (1,115) Al, ALFA, BETA
0012
            FORMAT ('OGIVEN (1-A; A; B):',3(F7.4,','))
       115
0013
            PA(1) = POL
0014
            PB(1) = P1L
0015
            PH≈ P1H+ 0.001
0016
            SP1= P1S
      C
0017
       116
            D≈ SP1/POS
0018
            DO 111 M= 1, 3
0019
                   DD= PB(M)/PA(M)
0020
                   IF (DD+0.01.LE.D.OR.DD-0.01.GE.D) GO TO 128
0022
                   IF (PB(M).GT.PH) GO TO 126
      C
0024
                   CALL GUNTHR (ALFA, PA(M), BETA, PB(M), SS(M), CC(M))
0025
                   CALL ARCSIN (ALFA, PA(M), BETA, PB(M), SS(M+3), CC(M+3))
0026
                   CALL NORMBI (ALFA, PA(M), BETA, PB(M), SS(M+6), CC(M+6))
      C
0027
                   IF (M.GE.3) GO TO 111
0029
                  PA(M+1) = PA(M) + POS
0030
                  PB(M+1) = PB(M) + SP1
0031
       111
            CONTINUE
      C
0032
            DO 122 Mm 1, 9
0033
                   I= SS(M)+ 0.5
0034
       122
                  SS(M) = I
0035
       117
            DO 121 Mm 1, 3
0036
                  DO 119 I= M, 9, 3
0037
                     CALL EXACT (SS(I),PA(M),CC(I),BO(I),N)
0038
       119
                     CALL EXACT (SS(I),PB(M),CC(I),B1(I),N)
0039
       121
           CONTINUE
0040
           WRITE (2,123) (PA(I),I=1,3),D,PB(1),SS(1),CC(1),PB(2),SS(2),CC(
                                       PB(3);SS(3);CC(3);D;PB(1);SS(4);CC(
           I
                                       PB(2);SS(5);CC(5);PB(3);SS(6);CC(6)
           T
                                       D:PB(1):SS(7):CC(7):PB(2):SS(8):CC(
                                       PB(3),SS(9),CC(9)
           FORMAT ('OMETHOD
0041
                                                  N',7X,'C
                              DNP1=()3(F8.4;(
          ĸ
                     BINOMIAL (,F6.1,3(F8.4,F8.1,F8.2)/
          Δ
                     ARCSINE (,F6.1,3(F8.4,F8.1,F8.2)/
                     NORMAL.
                             (1F6.1F3(F8.4FF8.1FF8.2))
           WRITE (1:125) (PA(I):I=1:3):D:PB(1):BO(1):B1(1):PB(2):BO(2):B1(
0042
                                       PB(3);B0(3);B1(3);D;PB(1);B0(4);B1(
```

```
SINGLE, SINGLE/LI:1 = SINGLE
           E.
                                          PB(2),BO(5),B1(5),PB(3),BO(6),B1(6)
            T
                                          D,PB(1),BO(7),B1(7),PB(2),BO(8),B1
                                          PB(3);80(9);81(9)
0043
            FORMAT ('OMETHOD
                                                                 1)/
                                 DNP1='+3(F8+4' P>1-A P<B
                     ' BINOMIAL', F7.1, 9F8.4/' ARCSINF ', F7.1, 9F8.4/
           M
                               'sF7.1:9F8.4)
                     ' NORMAL
0044
            PB(1)= PB(1)+ DS
0045
            SP1= (D4 0.5) *PA(2) -PB(1)
0046
            GO TO 116
      C
            BETA= BETA+ BS
0047
       126
0048
            IF (BETA-LE-BH) GO TO 114
0050
            BETA: BL
0051
            ALFA= ALFA+ AS
0052
            IF (ALFA-LE-AS) GO TO 114
0054
            WRITE (5,*)
            WRITE (5:*)'END OF ITERATIONS! END? CY/NJ'
0055
            A= 'Y'
0056
0057
            RETURN
0058
            WRITE (5:*)
       128
            WRITE (5,*)/DESCRIMINATION RATIO ERROR; D=(,D)( DD=(,DD
0059
0060
            A= 'R'
0061
            RETURN
```

0062

END

```
0001
             SUBROUTINE NORMAL (X; U; SD; ZTAB; TABZ)
      CC---
      CC
            PROGRAM: NORMAL PROBABILITY DISTRIBUTION APPROXIMATION
      CC
      CC
                       CUM. NORMAL= 1 - F(X) * (B1 * T + B2 * T**2 + B3 * T*
      CC
                                                         + B4 * T**4 + B5 * T*
                       MIN. ACCURACY: +- 0.000 000 075
      CC
      CC
      CC
            REF:
                   ABRAMOWITZ: M.: I. STEGUN: EDS. "HANDBOOK OF MATH.
      CC
                       FUNCTS. WITH FORMULAS, GRAPHS, AND MATH TABLES", APPL
      CC
                       MATH SERIES #55; WASH, DC, NAT'L BUREAU OF STDS., 196
      cc
      CC
            GIVEN:
                       X
                              SAMPLE STATISTIC
      CC
                       U
                              = DISTRIBUTION MEAN
      cc
                       SD
                              STANDARD DEVIATION
      CC
      CC
            COMPUTES: ZTAB
                              = NORMAL CUMMULATIVE PROBABILITY
      CC
                       TAR7
                              = (1 - ZTAB)
      CC---
            DATA B1/0.31938153/; B2/-0.356563782/; B3/1.781477937/; DUMY/0.
0005
                B4/-1.821255978/, B5/1.330274429/, CONST/0.39894228/
           7.
0003
            7= (X - U)/SD
            IF (Z.GE.O.) 60 TO 21
0004
0006
            Z = -Z
0007
            DUMY = 1.
8000
            T = 1./(1.+z *0.2316419)
       21
            C = 1/SQRT(2* 3.141526536); SEE DATA
0009
            F = C \times EXP(-(Z**2)/2.)
0010
            <u> ፐለክጀ = Fx (ክኒቱ T +ክ2x Txx2 +ክ3x Txx3 +ክ4x Txx4 +ክ5x Txx5)</u>
            IF (DUMY.EQ.O.) GO TO 23
0011
0013
            TABZ = 1.-TABZ
0014
       23
            ZTAB = 1.-TABZ
0015
            RETURN
0016
            END
```

```
1000
             SUBROUTINE REVNOR (X, U, SD, ZTAB, TABZ)
       CC---
       CC
             PROGRAM:
                        REVERSE NORMAL PROBABILTY DISTRIBUTION
       \mathbb{C}\mathbb{C}
       cc
                        Xm T = (CO+ C1*T+ C2* T**2)/(1+ D1*T+ D2* T**2+ D3* T*1
       CC
       CC
                        MIN. ACCURACY: +- 0.000 45
       CC
       CC
             RFF: HAISTINGS, CECIL UR, 'APPROXS FOR DIGITAL COMPS', PRINCET(
       CC
                        NJ, PRINCETON UNIV. PRESS, 1955.
       CC
             GIVEN:
       CC
                      U
                            = DISTRIBUTION MEAN
       CC
                      \mathbf{s}
                            ™ STANDARD DEVIATION
       cc
                      ZTAB - NORMAL CUMMULATIVE PROBABILITY
       CC
                      TABZ == (1 - ZTAB)
       CC
       CC
             COMPUTES: X
                            = POINT STATISTIC
       CC----
0002
             DATA CO/2.515517/; C1/0.802853/; C2/0.010328/; DUMY/1./;
                  D1/1.432788/, D2/0.189269/, D3/0.001308/
            Ţ
0003
             F= ZTAB
0004
             TABZ= 1- ZTAB
0005
             IF (ZTAB.GE.1) GO TO 35
0007
             IF (ZTAB-LT-0.5) GO TO 31
0009
             DUMY= 0.
0010
             F= 1.- ZTAB
        31
             TT= ALOG (1./F**2)
0011
0012
             T= SRRT (TT)
0013
             XN= CO+ C1* T+ C2* T**2
0014
             XD= 1.+ D1* T+ D2* T**2 +D3* T**3
0015
             X= T- XN/ XM
0016
             IF (DUMY.EQ.O.) GO TO 33
0018
             X::: -X
0019
       33
             X= X* SD+ U
0020
             GO TO 37
0021
       35
37
             X= 999.999
0022
             RETURN
0023
             END
```

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3-83

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